

ACTIVE VALVE CONTROL FOR CONTROLLED ENERGY RELEASE IN NON-LINEAR SEMI-ACTIVE DEVICES

**Sylvain Corman, J. Geoffrey Chase, Gregory A. MacRae,
Geoffrey W. Rodgers**

University of Canterbury, Christchurch, New Zealand

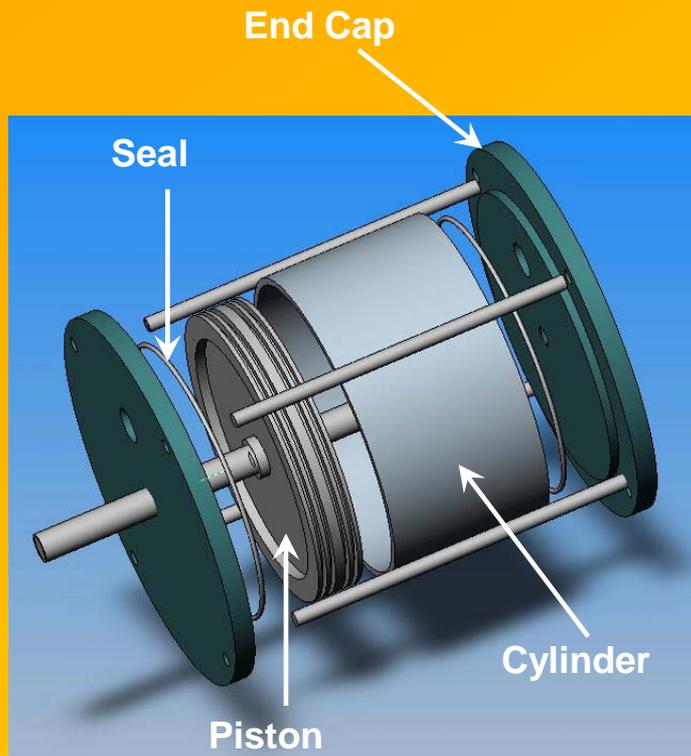


Motivation

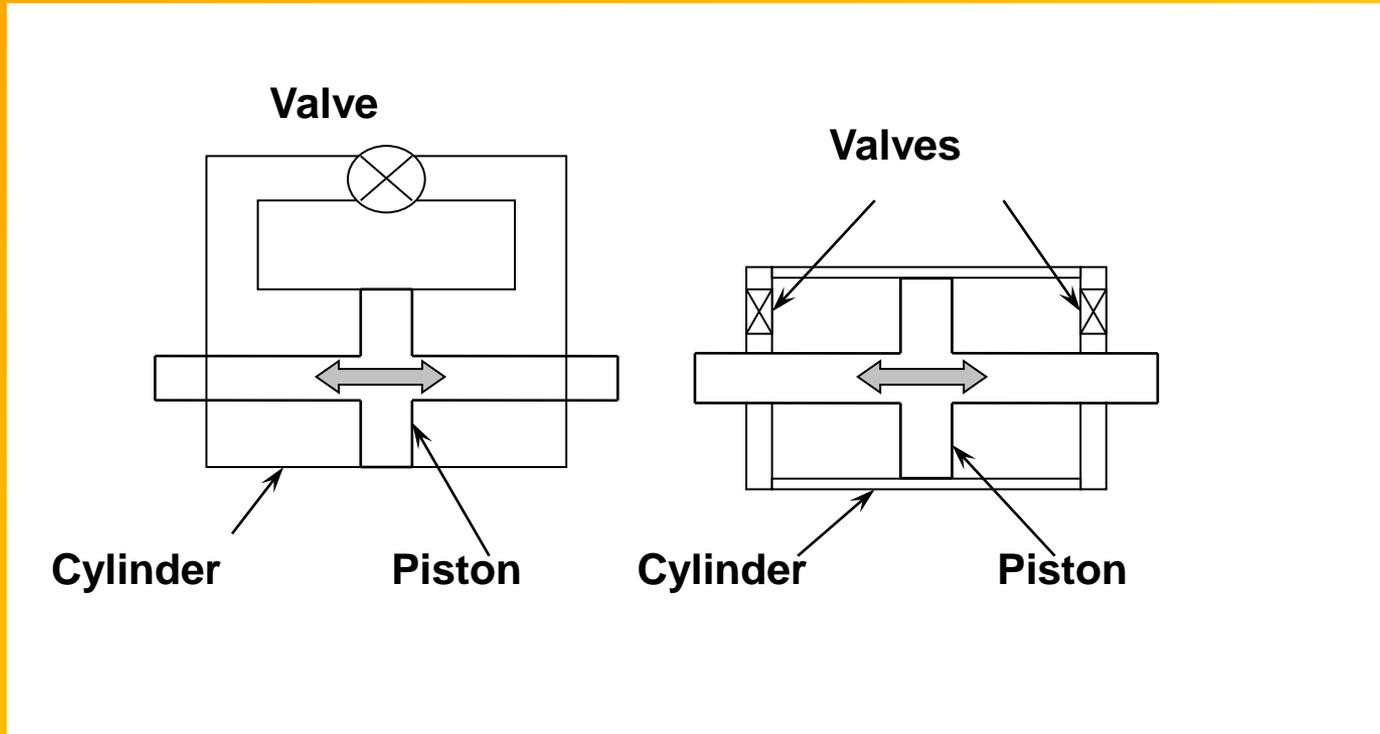
- *A main goal of a structure in a seismic event is to dissipate energy in a repeatable fashion*
- *Preferably in large amounts*
- *A diamond shaped resetable (Semi-Active) device has been shown to break existing compromises between reducing base shear and increasing dissipated energy with these devices*
- *HOWEVER, these solutions rely on an ideal linear shape for the device hysteresis loop → From a highly nonlinear device!*
- *This presentation presents a unique active valve control that provides this ideal, linearised shape using highly accurate, validated nonlinear device models [Mulligan et al, 2008; 2010]*

Re-Shaping Hysteretic Behaviour Using Semi-Active Resetable Devices

***Double-acting piston with controlled dissipation enables
customisation of structural hysteresis***

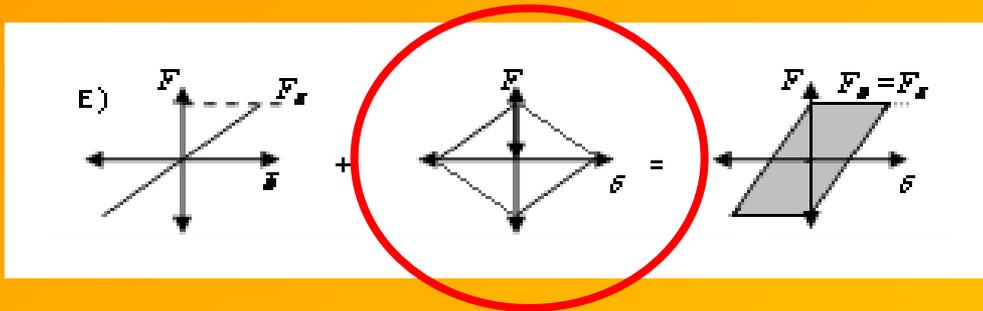


Device Design



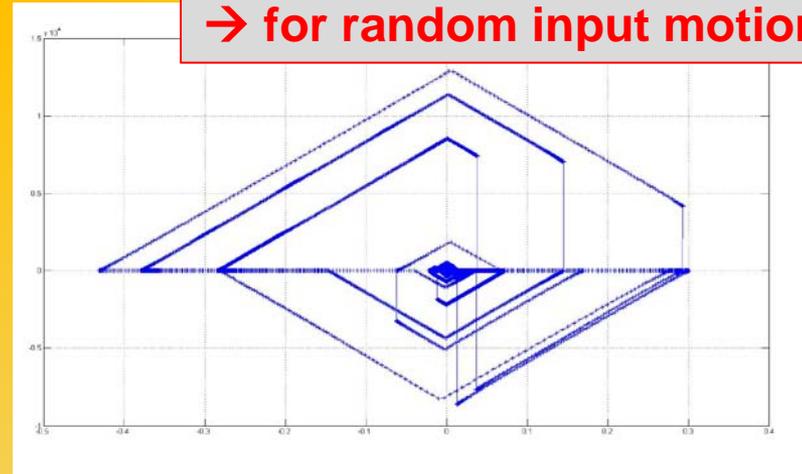
Independent two chamber design allows broader range of control laws

A Diamond-Shaped Solution



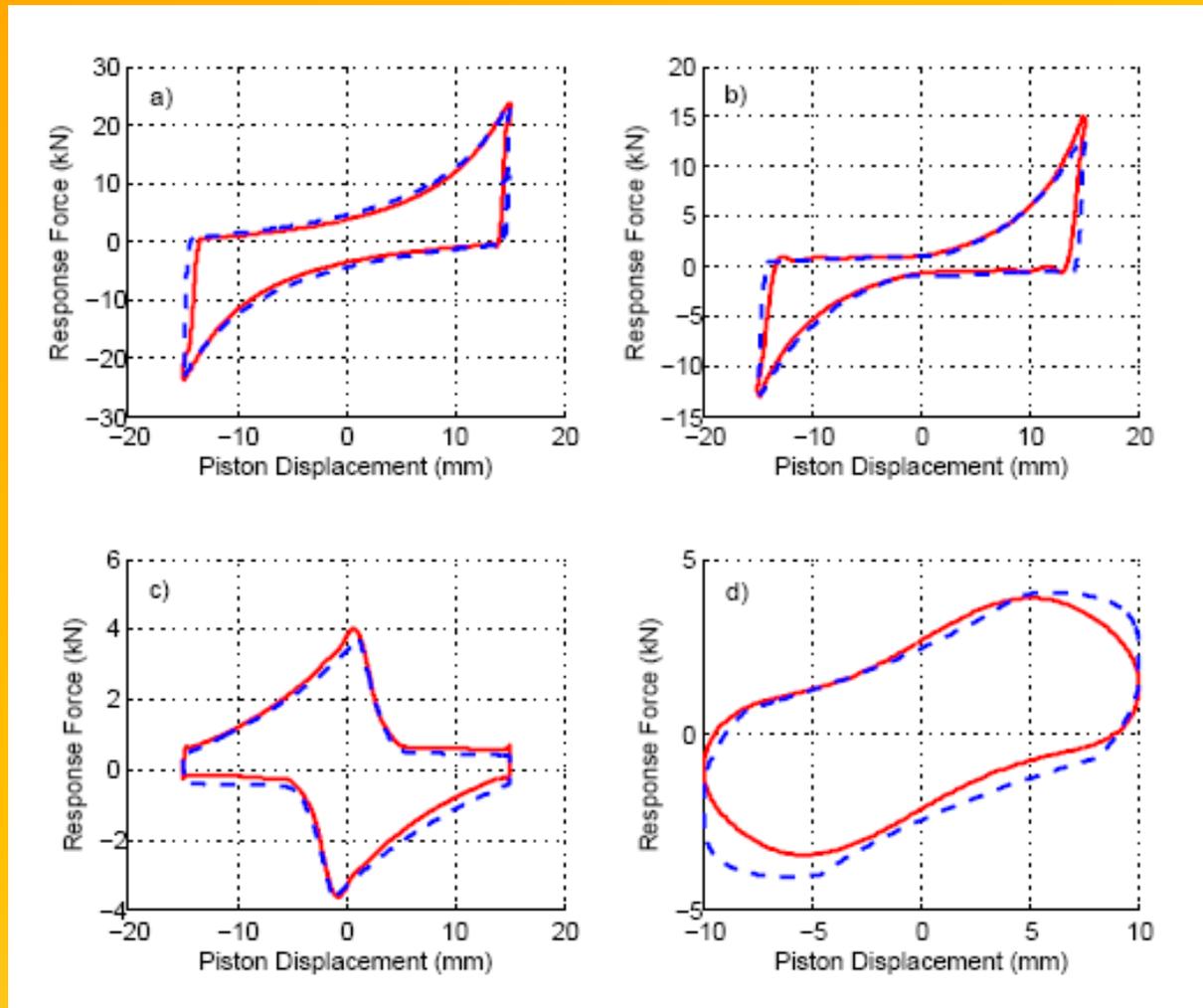
- **Increased** energy dissipation
- **No increase** to base shear
- **Reduced** displacement
- Meets all goals
- **Problem:** How to get this ideal linear behaviour from a nonlinear device

Ideal Device Model Loop
→ for random input motion



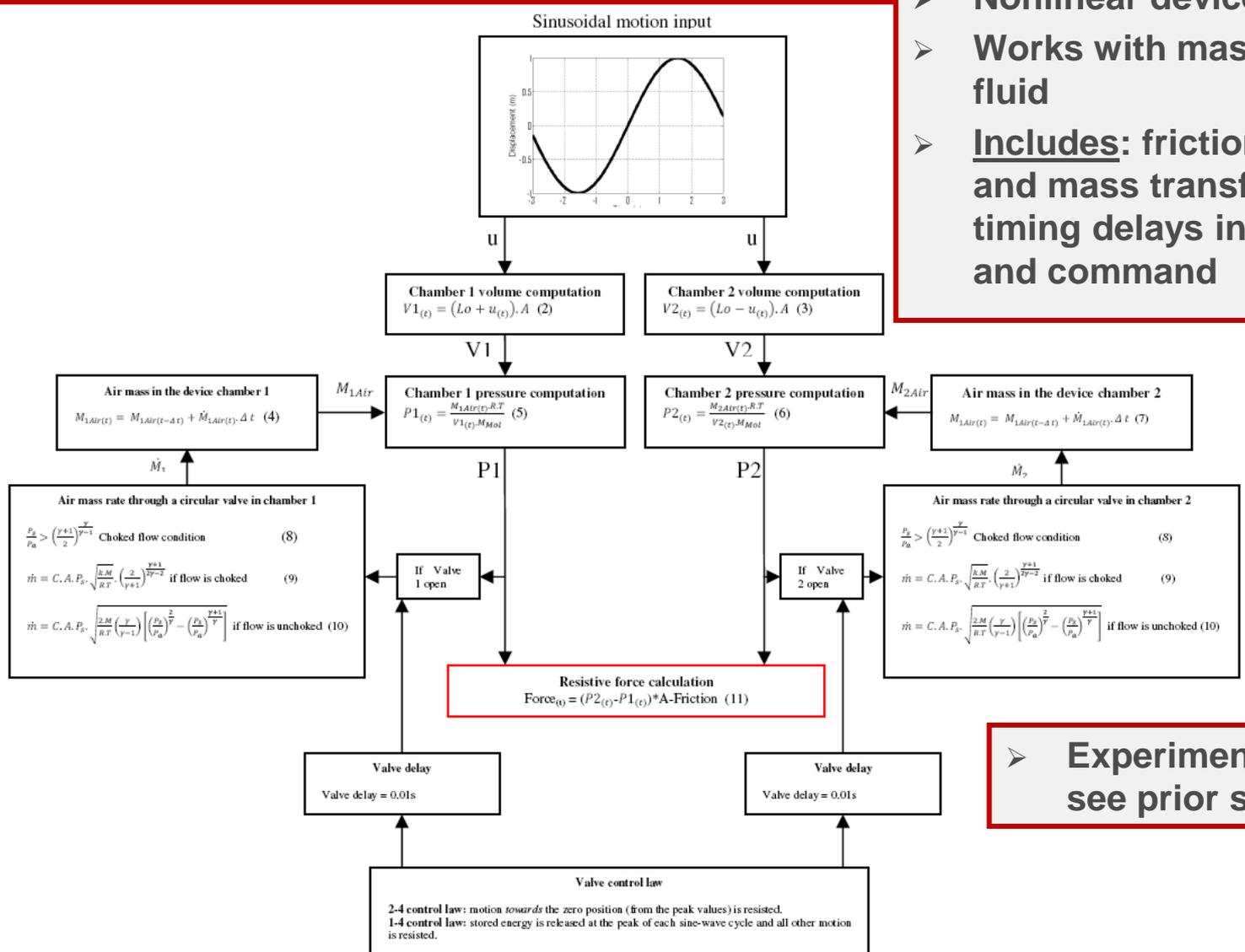
The Problem = Nonlinear Devices

- Typical device control laws yield nonlinear hysteresis loops:



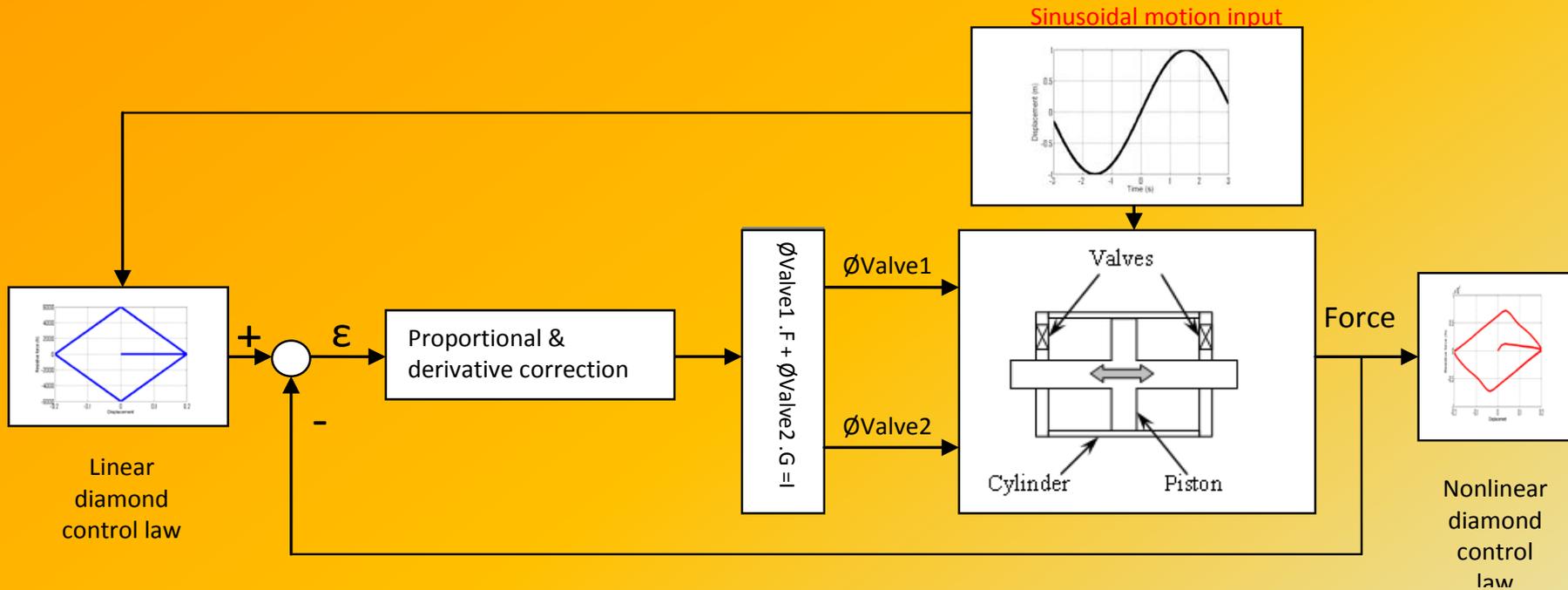
How Nonlinear? ... Very

- Nonlinear device model and flow
- Works with mass flows of working fluid
- Includes: friction, nonlinear heat and mass transfer, valve size, and timing delays in valve opening and command



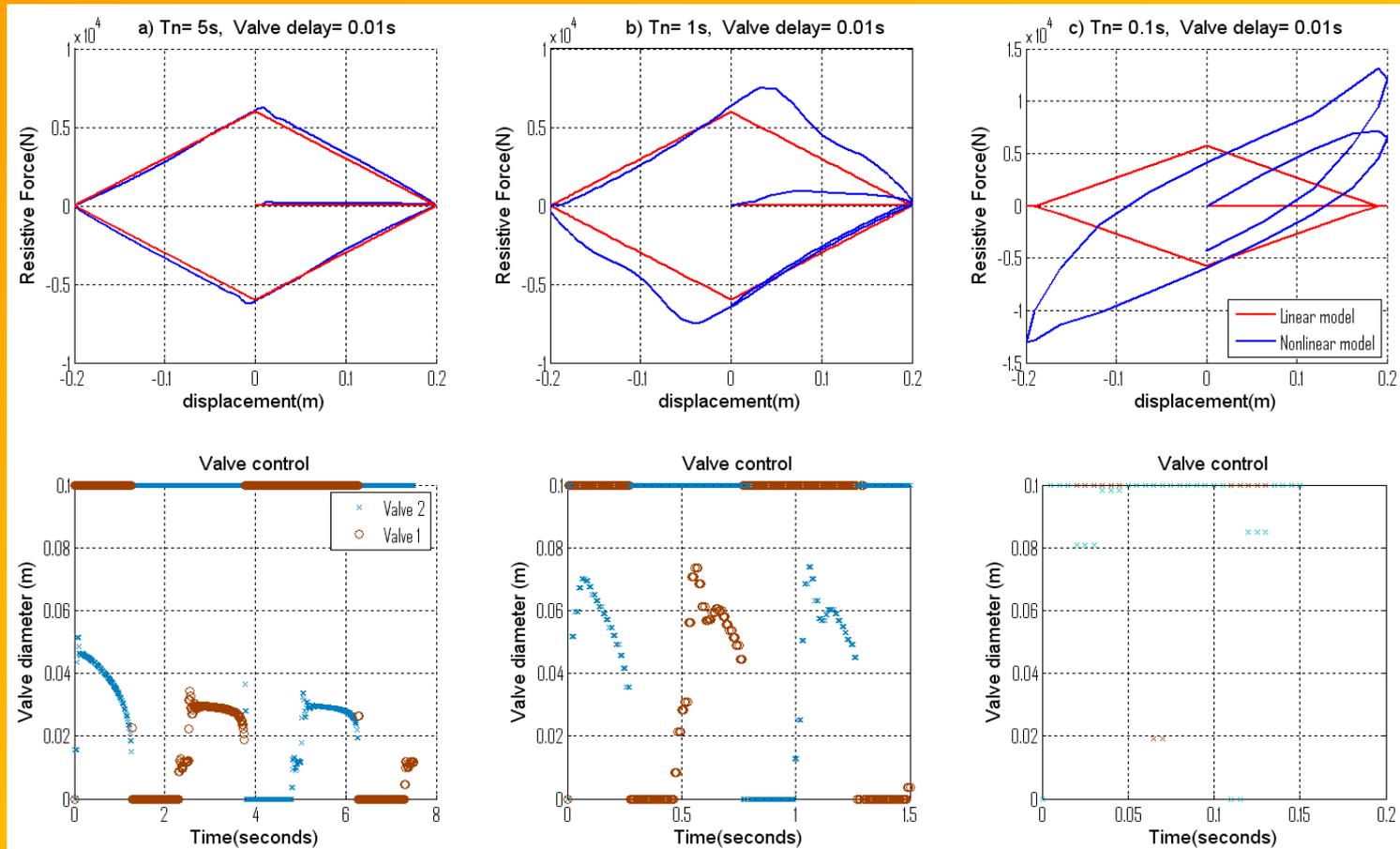
➤ Experimentally validated – see prior slide figure

Solution: Active Valve Control



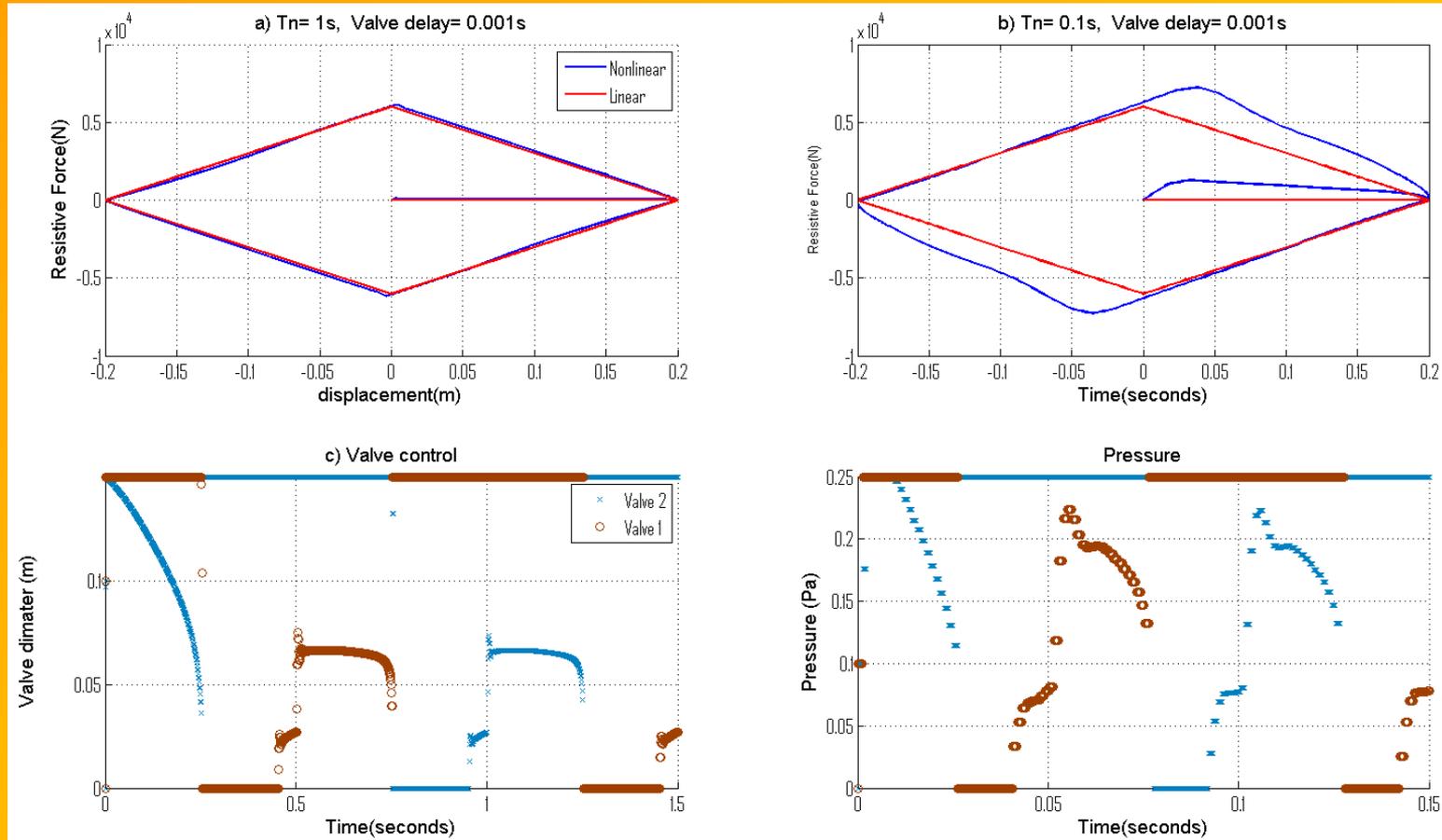
- **Feedback loop sets desired shape**
- **PD control used to set valve diameter as control input**
- **Tested with sinusoidal input motions (for clarity)**

Results vs Structure Period



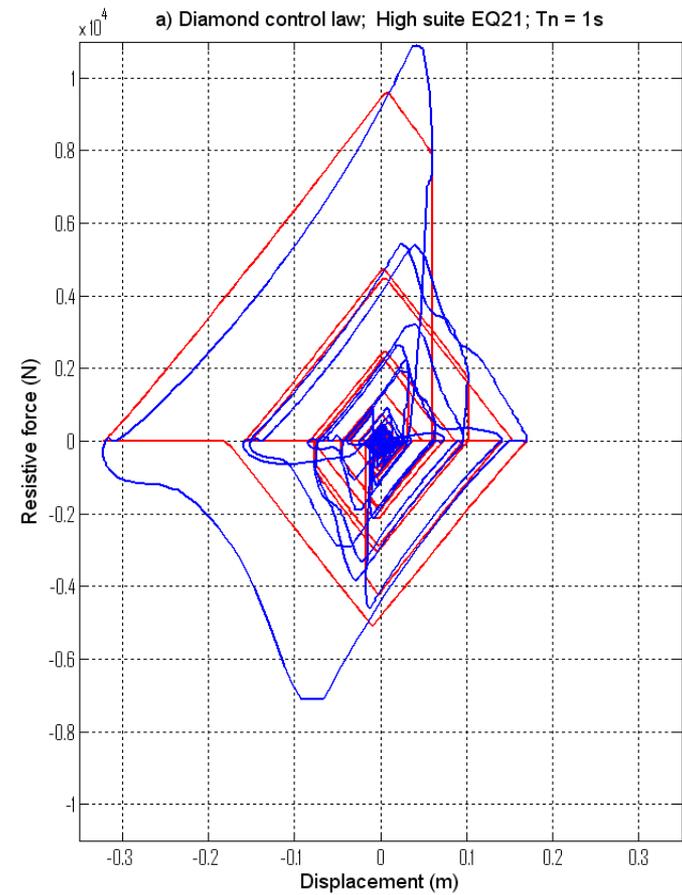
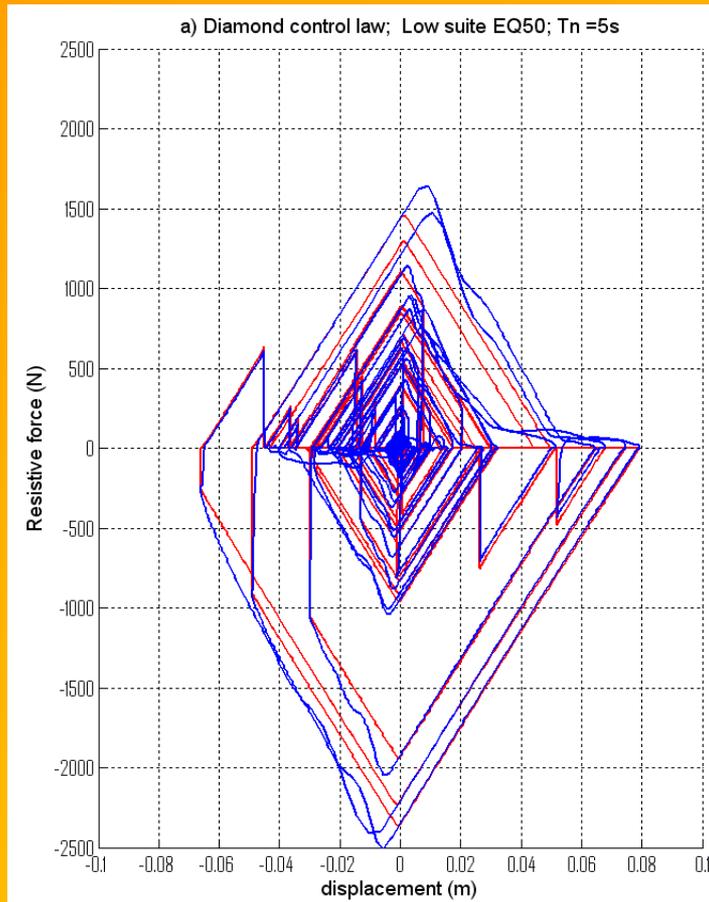
- As period shrinks the number of time steps to control shape per cycle declines significantly → Loss of control and inability to control shape
- At $T = 0.1$ sec with valve delay of 0.01 sec → Only 10 corrections are possible to control shape (100 for $T = 1.0$ sec and so on).

Results vs Valve Delay



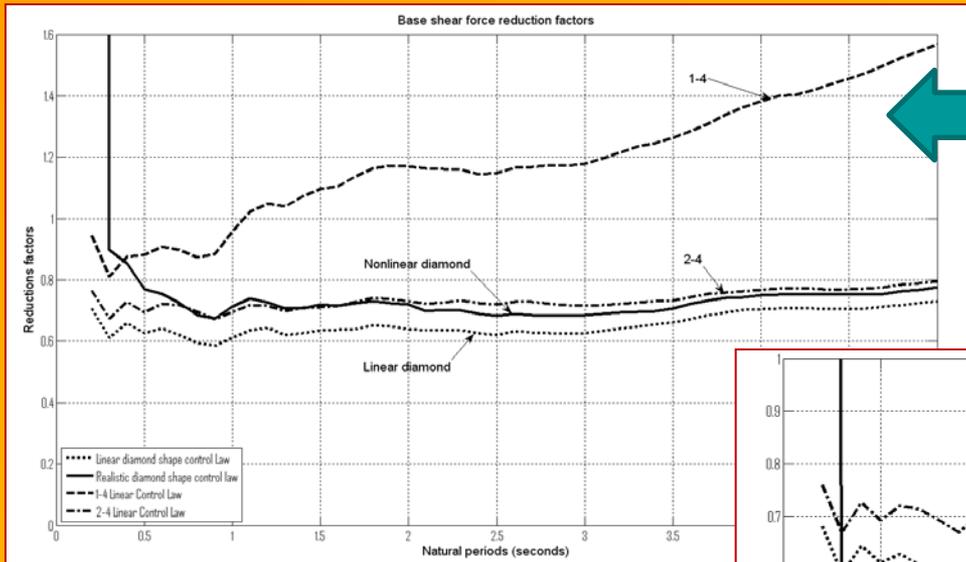
- Similar to changing period. Reduced valve delay provides more cycles to make corrections and achieve good control
- Valve delay and T_n trade off in design
- Realistic valve delays depend on valve size

Results – Realistic Input



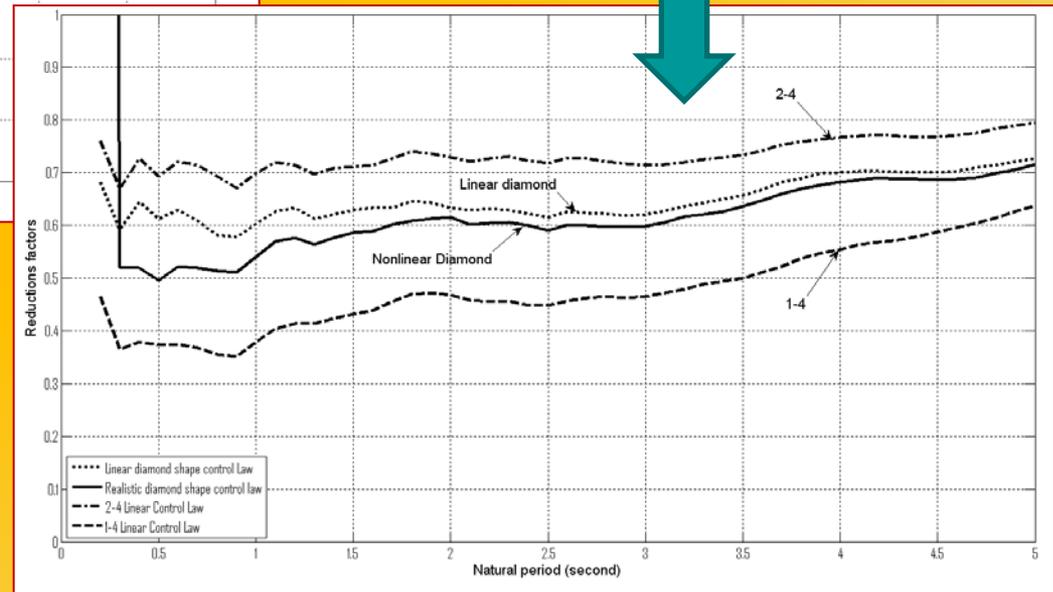
- SDOF spectral analysis case with $T_n = 5s$ and $1s$ (left / right)
- Actual system close to ideal linear except for 1-2 cycles at faster period
- Valve delay = $0.01s$

Results – Spectral Analysis



Structural Force
(and displacement)

Base Shear Force



→ Repeat of plots from first presentation comparing to 1-4 and 2-4 devices

- Spectral analysis across all 3 SAC suites with valve delay of 0.01s
- Ideal versus Nonlinear → Did we achieve the outcome of matching the linear, ideal case (robust over 60 ground motions)??
- At low T_n , valve delay → T_n and not a good match. OK after $T_n = 1.0-1.5s$

“Local” Conclusions

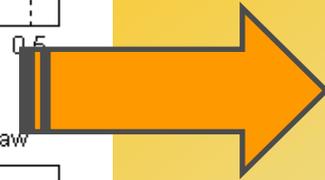
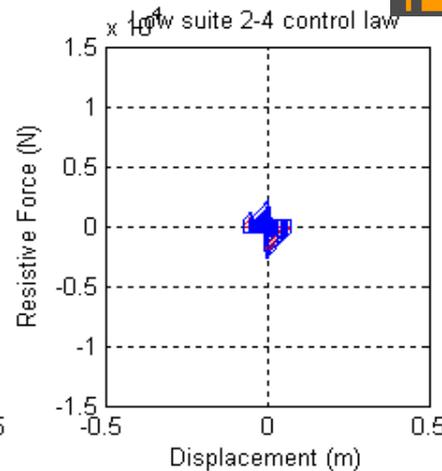
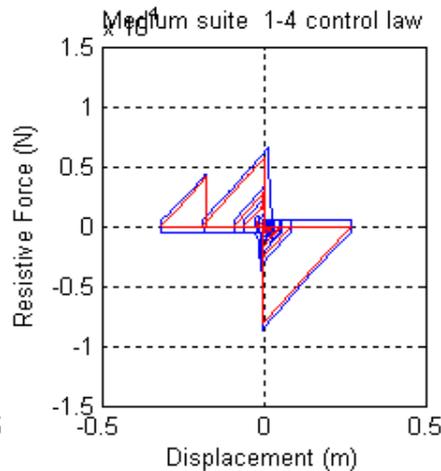
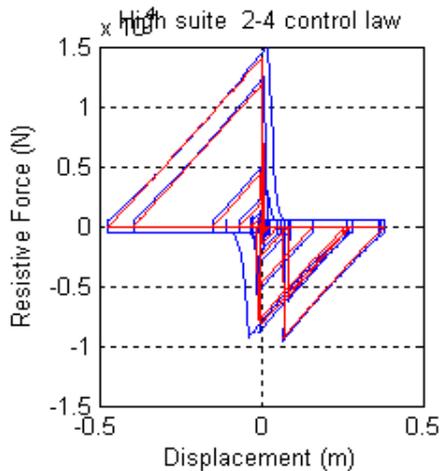
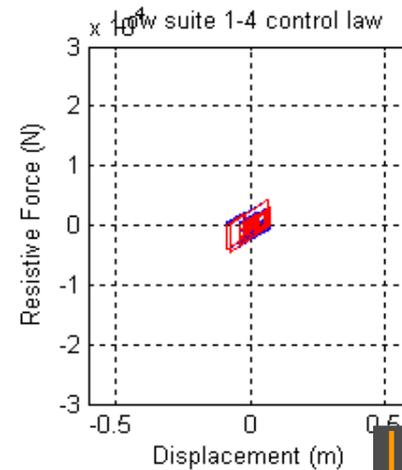
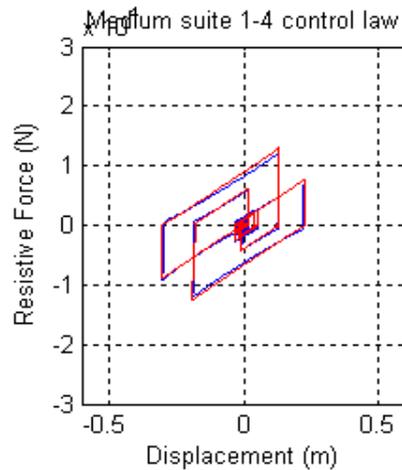
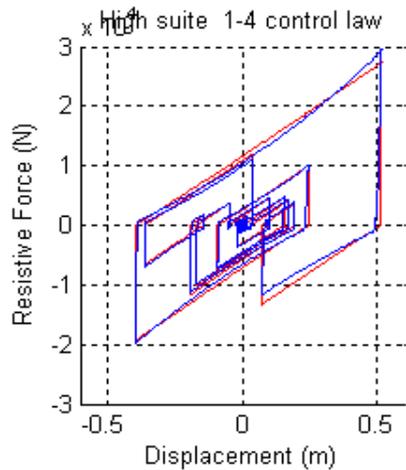
- Diamond shape active valve controlled resetable devices offer some significant potential for specific, high value applications
- Active valve control implemented using a validated, highly nonlinear model of semi-active devices
- Basic PD control can yield a highly linear, ideal device outcome for both sinusoidal and random earthquake (response) inputs
- Valve delay and natural period (T_n) must be considered in valve selection for obtaining desirable results
 - Tradeoff leads to selecting (e.g.) one large valve versus several smaller but faster valves to yield same total orifice area
- Spectral analysis shows the models and approach are robust over a wide range of periods and ground motions

So, ... From these 2 talks ...

- We can use resettable devices to further optimise hysteresis loops and maximise trade
- Accomplished by using active valve control to effectively “linearise” these devices
- When they act like a linear ideal device they are easily analysed, BUT also ideal (maximum) energy dissipaters
- But, could we do this passively by design alone for 1-4 and 2-4 devices that don't need active valve control?

The Real End ... OR What's to come

- But, could we do this passively by design alone for 1-4 and 2-4 devices that don't need active valve control?



YES

ACKNOWLEDGMENTS

This research was funded by the NZ Earthquake Commission (EQC) Research Foundation and the Foundation for Research Science and Technology (FRST)

