

1 Magnesium hydroxide is a sustainable material for CO₂ sequestration, according to an acid
2 digestion and electrolysis method using olivine-rich silicate rocks in a fully recoverable
3 system.

1 **Transformation of abundant magnesium silicate minerals for enhanced**
2 **CO₂ sequestration**

3

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18

19 **Abstract:**

20 **Global climate change related to anthropogenic CO₂ emissions is one of the most**
21 **significant challenges for the future of human life on Earth. There are many potential**
22 **options for reducing or even eliminating atmospheric CO₂ emissions including**
23 **underground sequestration, carbon mineralization and ocean storage. One of the most**
24 **promising materials for carbon mineralization is Mg(OH)₂ which is highly reactive and**
25 **capable of forming stable carbonates. Here we show a novel low-carbon method of**
26 **producing Mg(OH)₂, from globally abundant olivine-rich silicate rocks. A combination**
27 **of acid digestion and electrolysis of olivine were used to produce Mg(OH)₂ in a fully**
28 **recoverable system. The use of Mg(OH)₂ from olivine provides a viable pathway for**
29 **significant industrial scale reductions in global anthropogenic greenhouse gas emissions.**

30

31 **Introduction:**

32 The effects of unchecked CO₂ emissions on global climate change are being
33 increasingly seen and felt across the world. Examples of issues include increased land and sea
34 temperatures, glacier and sea ice loss, and sea level rise (1). Urgent action is needed to limit
35 future emissions and sequester existing atmospheric CO₂ in order to circumvent issues related
36 to global warming (2). In 2018, ~37 billion tonnes of CO₂ was released into the atmosphere
37 (3). Point source emissions such as power generation and industrial production account for
38 approximately 60% of the total CO₂, but this is expected to decrease to 50% by 2050 (4).

39 Methods for long-term storage of CO₂ can be classified as either underground
40 sequestration or carbon mineralization, of which underground sequestration in sedimentary
41 formation is considered the most mature technology (5). Carbon mineralization can be further
42 divided into 3 approaches: 1) *ex-situ*, where material is transport to the site and reacted with
43 CO₂ typically at elevated temperatures and pressures, 2) *surficial*, using dilute or

44 concentrated CO₂ and 3) *in-situ*, where the CO₂ is transported to site with suitable geological
45 formations, typically containing serpentine or olivine-bearing basalts (5). Ocean storage has
46 also been proposed as a potential means of CO₂ sequestration, but comes with a number of
47 environmental consequences (4).

48 A number of materials have been proposed for carbon mineralization including
49 serpentine, olivine, wollastonite, magnesium oxide and magnesium hydroxide (6-10). Of the
50 various materials which may be suited for transport to the emissions source, Mg(OH)₂ is one
51 of the most reactive for carbonization (5). Aqueous carbonation of Mg(OH)₂ can result in the
52 formation of a hydrated Mg-carbonate such as nesquehonite (MgCO₃·3H₂O), dypingite
53 (Mg₅(CO₃)₄(OH)₂·5H₂O), and hydromagnesite (Mg₅(CO₃)₄(OH)₂·4H₂O) under atmospheric
54 or near atmospheric conditions (11). The formation of magnesite (MgCO₃) is also possible
55 but this typically requires higher temperatures (>100 °C) and pressures above 100 bar.
56 Seeding Mg(OH)₂ slurries with magnesite at elevated pressures and temperatures has been
57 shown to produce a stable anhydrous magnesite (12). One of the benefits of Mg(OH)₂ with
58 regard to overall conversion rates and transportation is that it does not contain significant
59 quantities of unreactive material, such as silica or iron which are typically found in olivine or
60 serpentine.

61 MgO and Mg(OH)₂ are usually sourced from either the calcination of magnesite or
62 precipitated from Mg-rich brines and sea water (13). Recovery of Mg(OH)₂ from seawater
63 has the potential to provide virtually limitless supplies of the material; however, its
64 commercial production typically requires the use of lime, which itself has significant
65 embodied CO₂, resulting in little overall environmental benefit. The high temperature
66 pyrohydrolysis process of using MgCl₂·6H₂O to form MgO and HCl (14) could potentially
67 provide a low carbon Mg(OH)₂ alternative; however, concentrations of Mg-chloride in

68 seawater are relatively low which limits the efficiency of the process unless highly
69 concentrated brines are used.

70 Magnesium-rich silicate minerals, such as olivine ((Mg,Fe)₂SiO₄), in ultramafic and
71 mafic rocks have the potential to produce reactive Mg(OH)₂ with zero CO₂ emissions. Until
72 now, Mg(OH)₂ recovery from olivine has not been used primarily because of the slow rate of
73 hydration (i.e., serpentinization)(15, 16) or ultramafic mineral extraction efforts have been
74 focused on silica recovery (17) rather than Mg(OH)₂ production. Furthermore, a satisfactory
75 energy efficient industrial process has not been developed yet (18).

76 Here, we extract Mg(OH)₂ directly from olivine using a combination of acid digestion
77 and electrolysis. The acid used in the digestion process is completely recoverable and
78 provides a source of usable energy. Recovered Mg(OH)₂ was found to have a similar level of
79 reactivity compared to commercially available Mg(OH)₂. A slurry of recovered Mg(OH)₂ and
80 water was shown to effectively sequester CO₂ forming a hydrated Mg-carbonate. In addition
81 to Mg(OH)₂, amorphous silica, which has the potential for use as a partial cement
82 replacement, was also recovered from the olivine.

83

84 **Methods: Synthesis of Mg(OH)₂**

85 The synthesis of Mg(OH)₂ uses olivine from ultramafic rocks and/or olivine-rich
86 basalts as the raw material and source of magnesium (**Fig. 1**). Olivine is sparingly soluble
87 under standard state conditions with a total Mg concentration of less than 6 mg L⁻¹ resulting
88 in excessive energy demands for the recovery process. As the pH of the reaction solution
89 decreases, the solubility of Mg increases considerably. In our investigation, 100 g of finely
90 ground forsteritic ((Mg_{0.9}Fe_{0.1})₂SiO₄) olivine (19), with a mean particle size of 28 μm, was
91 combined with 500 ml of 2 M HCl, resulting in the formation of a solution containing MgCl₂
92 and FeCl₂ and SiO₂. The silica is produced through a process of hydrolysis and subsequent

93 polymerization and condensation of silicic acid ($\text{Si}(\text{OH})_4$). Strong acids such as HCl are
94 known to accelerate the hydrolysis process, whereas, a high pH favours the polymerization
95 and condensation process that is supported by the addition of $\text{Mg}(\text{OH})_2$ in this study. Here the
96 pH of the solution increased rapidly from less than 0 to ~ 3 after 4 hours of mixing at 20 °C.

97 The concentration of Mg^{2+} in solution was determined by complexometric titration
98 used to measure total hardness of water. 1 ml of sample solution was added in a conical flask
99 containing 10 ml of 0.05 M ethylenediaminetetraacetic acid (EDTA) solution and 10 ml of
100 ammonia buffer solution. Eriochrome black T was used as an indicator. The solution was
101 titrated using a 0.025 M magnesium chloride solution until its colour changed from blue to
102 pink. The concentration of complexed EDTA solution was used to determine the magnesium
103 ion concentration. Since the concentration of calcium ions in the sample solution was
104 negligible, it was assumed that all the ions complexed with EDTA were magnesium. The Mg
105 concentration was found to be $\sim 24 \text{ g L}^{-1}$, which is more than 19 times the concentration of
106 Mg in seawater and over three orders of magnitude greater than the concentration resulting
107 from serpentinization reactions involving pure water. The potential Mg extraction efficiency,
108 therefore, is considerably higher using an acid digestion solution than it is from seawater.

109 Once the initial digestion phase was completed the solution was allowed to settle for 1
110 hour after which it was decanted to separate the solution containing the Mg, Fe and Si ions
111 from any unreacted olivine (**Fig. 1**). Silica was precipitated from solution by increasing the
112 pH to >3.5 through the addition of 1 g of $\text{Mg}(\text{OH})_2$. The pH of the remaining solution was
113 further increased to almost 7 to precipitate the dissolved iron using 0.32 g of NaOH. The
114 silica and iron were separated from the solution using a centrifuge in this proof of principal
115 testing, whereas, an industrial filtration system would be used in practice. It should be noted
116 that the formation of gel-like products during the precipitation of silica and iron can cause
117 challenges to any filtration system. Regular flushing and cleaning of the membranes would be

118 necessary and likely require a number of cross flow filters, such as those used for silica
119 removal from geothermal waters, to be run in parallel to maintain operations. An alternative
120 approach and potentially more efficient method for the removal and recovery of the silica and
121 iron is by precipitate flotation.

122 The $MgCl_2$ solution was electrolysed in an H-cell with a carbon anode and platinum
123 cathode. A DC power supply was used to generate a current of approximately 100 mA
124 resulting in the formation of Cl_2 gas at the anode and H_2 gas at the cathode. $Mg(OH)_2$ was
125 formed at the cathode where the pH of the solution increased rapidly to ~ 9.5 . The recovered
126 $Mg(OH)_2$ was placed in a drying oven at $105\text{ }^\circ C$ for 1 day after which it was analysed by
127 scanning electron microscope (SEM), thermo gravimetric analysis (TGA) and X-ray powder
128 diffraction (XRD). For the commercial production of $Mg(OH)_2$, H_2 and Cl_2 would be
129 combined to produce HCl for re-use and as an energy resource, as is typically done in the
130 chemical process and manufacturing industry.

131

132 **Results and Discussion**

133 From this process, a total of 35 g of $Mg(OH)_2$ was produced from 100 g of olivine,
134 with 1 g of $Mg(OH)_2$ added in the silica precipitation stage. Approximately 5 g of iron oxide
135 was precipitated with the addition of 0.32 g of NaOH, which represented less than 1 % of the
136 total $Mg(OH)_2$ recovered. 35 g of amorphous silica was also recovered from the precipitation
137 stage. The SEM image and TGA graph provided in **Fig. 2 a,b** show the material recovered
138 after electrolysis was primarily $Mg(OH)_2$. XRD results provided in **Fig 2c.** show the
139 recovered silica was predominantly amorphous SiO_2 with some residual unreacted olivine
140 and confirm the material recovered after electrolysis was predominately $Mg(OH)_2$. The
141 composition of the raw olivine sand, recovered $Mg(OH)_2$, and recovered silica from olivine,

142 determined by X-ray fluorescence (XRF), are provided in **Table 1** and are consistent with the
143 other material characterization analysis.

144 In addition to the primary recovered $\text{Mg}(\text{OH})_2$, secondary materials of iron hydroxide
145 and silica may also be of use. The iron hydroxide for instance could be used as a high purity
146 raw material for iron production or as an absorbent while the amorphous silica can be used as
147 a partial replacement for Portland cement, in the production of concrete, which is a
148 significant industrial contributor to global CO_2 emissions (20). Our approach provides an
149 almost completely closed system for the production of $\text{Mg}(\text{OH})_2$ with the only additions
150 being olivine, as the source of Mg, and minor amounts of NaOH.

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152 **CO_2 and energy implications of Mg-hydroxide extraction**

153 Overall, conversion of olivine into $\text{Mg}(\text{OH})_2$ produces no direct CO_2 emissions and
154 the HCl used for digestion was completely recoverable. The large scale and industrial use of
155 strong acids such as HCl have serious consequences if released into the environment.
156 However, this is only an issue if there is a loss of containment from the process. The large
157 scale handling of HCl without loss of containment is well established in the chemical process
158 industries due to its use in commodity materials such as the manufacture of PVC and pickling
159 of steel. What is most important is that neither HCl nor chlorine leave the process described
160 in our work, as they are recycled within the process.

161 The total energy required, including quarrying and grinding, to produce $\text{Mg}(\text{OH})_2$
162 from olivine was calculated to be $6.28 \text{ GJ tonne}^{-1}$ (see **Fig. 1** and **Supplementary Methods**
163 for energy determinations and calculations). Further refinement of the process may allow
164 greater use of recovered $\text{Mg}(\text{OH})_2$ for pH control, a decrease in the total energy required, and
165 a reduction in NaOH. The $\text{Mg}(\text{OH})_2$ could be further processed into MgO but for CO_2
166 sequestration; however, $\text{Mg}(\text{OH})_2$ is known to be a faster reactant than MgO (10).

167 For every tonne of CO₂ sequestered as a Mg-carbonate, including nesquehonite and
168 hydromagnesite, 1.3 tonnes of Mg(OH)₂ is required, resulting in an energy consumption 8.17
169 GJ tonne⁻¹ of CO₂ (**Fig. 1**, see **Supplementary Methods** for calculations). Using the method
170 outlined in this paper would result in a net negative CO₂ emission, even if coal was used to
171 provide the necessary energy, though at ~25% sequestration efficiency. The overall carbon
172 sequestration benefits would improve substantially if a low carbon energy sources, or even a
173 mixed electrical supply, was used. For example, in California where roughly 50% of the
174 electricity is from non-fossil fuels , ~500 kg of CO₂ would be emitted for every 1,000 kg of
175 CO₂ captured and turned into Mg-carbonate.

176 To confirm the ability of the recovered Mg(OH)₂ to sequester CO₂, a Mg(OH)₂ water
177 slurry was pressurized to 4 bar with concentrated CO₂. Over a 48 hour period more than 50%
178 of the Mg(OH)₂ was converted to a hydrated Mg-carbonate, demonstrating the potential
179 conversion of CO₂ into a solid. The reactivity of the recovered Mg(OH)₂ was also confirmed
180 by the rapid increase in pH to ~10.5 when it was added to de-ionized water. As previously
181 noted, there are a number of other methods for sequestering CO₂ with Mg(OH)₂ using either
182 aqueous (12,21) or direct solid-gas reaction methods (10). Our proposed process has the
183 potential to provide a substantial source of energy efficient, low-carbon Mg(OH)₂ for use in
184 various carbon sequestration techniques currently being developed by other investigators.

185

186 **Olivine resources and feasibility**

187 Ultramafic rocks, enriched in olivine, constitute ~1% of Earth's terrestrial landscape,
188 a high proportion of oceanic crust, and >50 % of the upper mantle (22). Olivine-rich deposits
189 (**Fig. 3**) are primarily present within populated areas of the Circum-Pacific and
190 Mediterranean regions (23, 24). Olivine is present in many rocks such as basalt and other
191 ultramafics. We would like to note that although olivine was assessed and used in this study,

192 its metamorphic equivalent, serpentine ($\text{Mg}_3\text{Si}_2\text{O}_5(\text{OH})_4$) with its high reactivity in HCl and
193 worldwide deposits, could expand the scope and implications of this study. Our preliminary
194 investigations have shown Mg can also be extracted from basalt; however, we will primarily
195 focus our discussion on two enriched and accessible olivine deposits: the Semail ophiolite
196 (Oman) and the Red Hills Ultramafic Complex (New Zealand) which conservatively contain
197 1.4×10^5 and 871 billion tonnes of olivine, respectively (see **Supplementary Methods** for
198 sources and estimate calculations).

199 Using $\text{Mg}(\text{OH})_2$ to remove and sequester anthropogenic CO_2 estimated for 2020 (40
200 billion tonnes) in a Mg-carbonate would require ~105 billion tonnes of olivine. Reducing
201 global atmospheric CO_2 levels by an additional 10 billion tonnes would necessitate a further
202 26 billion tonnes of olivine. The sum of olivine required to do all of this would be 131 billion
203 tonnes; 0.1 % of the Oman ophiolite or 16 % of Red Hills, New Zealand (**Fig. 3**). To
204 sequester all anthropogenic CO_2 , these two deposits would last on the order of nearly a
205 decade (Red Hills) to one thousand years (Semail), assuming the deposits contained at least
206 60% olivine. The degree of serpentinization of each deposit and abundance of other minerals
207 such as ortho- and clinopyroxene would affect the overall extraction efficiency. Smaller
208 deposits, compared to the Semail ophiolite or Red Hills, around the world could significantly
209 aid the global reduction of anthropogenic CO_2 .

210

211 **Implications**

212 The concept of using ultramafic rocks and its metamorphic equivalents as sources of
213 Mg for CO_2 sequestration has been considered for at least two decades. However, one
214 limitation with regards to previous and current approaches is related to the distance between
215 the CO_2 gas source and the ultramafic site. Currently, concentrated CO_2 is being
216 transported/piped to ultramafic sites to be directly injected into the subsurface. Although

217 ultramafic sites are around the world, many are not sufficiently close to areas of high CO₂-
218 producing industries. Our approach allows bulk Mg(OH)₂ to be transported more efficiently
219 to locations/industries where it can be used on site for point source emissions control. For
220 example, transporting enough Mg(OH)₂ to sequester 1 tonne of CO₂, from its production
221 location to a point source such as a cement plant 1,000 km away by rail, would result in 37 kg
222 of CO₂ emissions (25).

223 Additionally, slight modifications to this approach through the further refinement of
224 Mg(OH)₂ to MgO has the potential to produce construction materials such as Mg-masonry
225 blocks (26) rather than simply burying the CO₂. There is considerable interest in the potential
226 use of MgO as an alternative to traditional Portland cement (13); however, there are a number
227 of issues which must be addressed, including: the low pH of the pore solution, which makes
228 its use in steel reinforced structures challenging, and high water demand which makes
229 handling more difficult. One of the major environmental issues associated Mg-based cements
230 is the vast majority of MgO is produced from MgCO₃ which results in the release of CO₂ at a
231 similar proportion to that of Portland cement. The alternative of recovering MgO from sea
232 water, as previously noted, also has considerable embodied CO₂ due to the use of CaO,
233 sourced from carbonates, in the recovery process. If MgO is to be used as a construction
234 material then a low carbon mineral extraction approach will be needed. The scale and scope
235 to mitigate climate change using Mg-bearing minerals from ultramafic and mafic rocks is
236 massive, but our experiments and others support that this is feasible.

237 Scaling up and improving efficiencies with regards to the processes described and
238 proven here will require a significant development and industrialization effort. We anticipate
239 that the engineering challenges to produce Mg(OH)₂ for use in CO₂ sequestration, as shown
240 in **Fig. 1**, are comparable to other well known industrial processes. One of the great
241 challenges, however, is how to use the billions of tonnes of carbonate produced to offset

242 anthropogenic CO₂ emissions and this requires further circumspection. A more realistic and
243 efficient approach to addressing global warming is to reduce CO₂ emissions. Until then, we
244 have demonstrated a process that is feasible and globally communal where many countries
245 and industries can participate. Overall, the recovery of magnesium hydroxide from olivine-
246 rich (and potentially serpentine-rich) rocks provides the basis for a direct route to reduce
247 global anthropogenic CO₂ and its associated climate change impacts.

248

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253 Employment, New Zealand (1708) to this project.

254

Figures and Tables

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256

257 **Figure 1: Simplified mineral extraction and carbon sequestration.**

258 Energy requirements are shown where $E_1 = 0.32$, $E_2 = 6.6$ and $E_3 = -0.64$ GJ tonne⁻¹ of
259 Mg(OH)₂ produced. Energy consumption details are provided in **Supplementary Methods**.

260 Note: Direct solid-gas carbon mineralization is also possible and the most likely approach for
261 point source CO₂ sequestration.

262 *Note: The carbonation product is likely to be hydrated Mg-carbonate such as nesquehonite,
263 dypingite, or hydromagnesite, but MgCO₃ formation is also possible depending on reaction
264 conditions (27).

265

266 **Figure 2: Characterization of recovered material.**

267 **a)** SEM image of recovered Mg(OH)₂ from electrolysis of olivine digestion solution, **b)** TGA
268 of recovered Mg(OH)₂ from olivine, **c)** XRD of recovered Mg(OH)₂ and of recovered silica
269 (B: brucite, L: lizardite, F: forsterite).

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271 **Figure 3: Distribution of ultramafic rocks and olivine lifetime estimates.**

272 The general distribution of ultramafic rocks (including peridotites and serpentinites) is shown
273 worldwide. Ultramafic rock distributions are based on location data from Oze et al. (24) and
274 compared to Real and Vishal (23). Please note that more ultramafic rock deposits are present
275 than shown and that the squares do not represent particular sites. The billions of tonnes of
276 olivine per year needed to sequester all anthropogenic CO₂, and reduce global atmospheric
277 CO₂ as well as the lifetime supply of olivine from the Red Hills (New Zealand) and Semail
278 Ophiolite (Oman) is shown and based on calculations provided in the **Supplementary**
279 **Methods**.

280

281 **Table 1.** Elemental compositions of raw olivine sand and recovered Mg(OH)₂ and silica from
282 olivine, determined by XRF analysis.

	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	Na ₂ O	K ₂ O	LOI	Total
	-----Wt. %-----								
Raw olivine	39.6	0.38	10.7	0.73	45.0	0.14	0	3.2	100.0
Mg(OH) ₂ -olivine	0.1	0.11	6.4	0.30	60.4	0.03	<0.01	32.3	99.9
Silica-olivine	63.2	0.23	4.7	0.57	13.9	0.03	0.06	16.4	99.0

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305 **Data Availability**

306 Data files containing XRD and TGA results of the recovered materials from this investigation

307 are available from the figshare data set repository: DOI 10.6084/m9.figshare.13543091.

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330 **Author Contributions**

331 **AS:** Conceptualization, Methodology, Resources, Formal Analysis, Funding Acquisition,

332 Writing-original draft, **VS:** Conceptualization; Methodology, Formal Analysis, Investigation,

333 Writing-review, **CO:** Conceptualization; Writing-review & editing, **BS:** Investigation,

334 Methodology, **CC:** Writing-review & editing, **NY:** Investigation, Methodology, **MW:**

335 Conceptualization, Writing-review & editing, **AM:** Conceptualization, Writing-review &

336 editing

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339 **Competing Interests**

340 All authors declare no competing interesting

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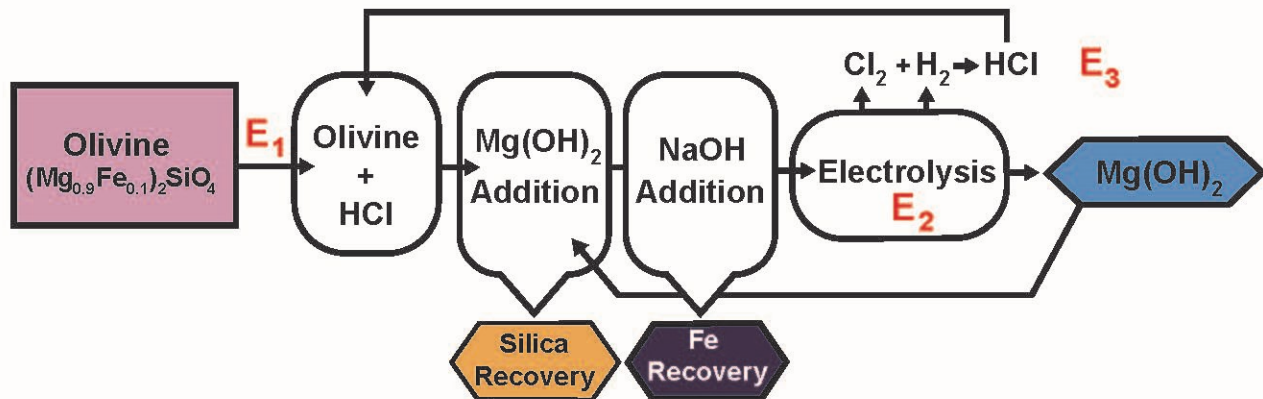
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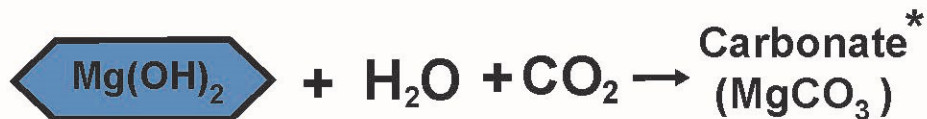
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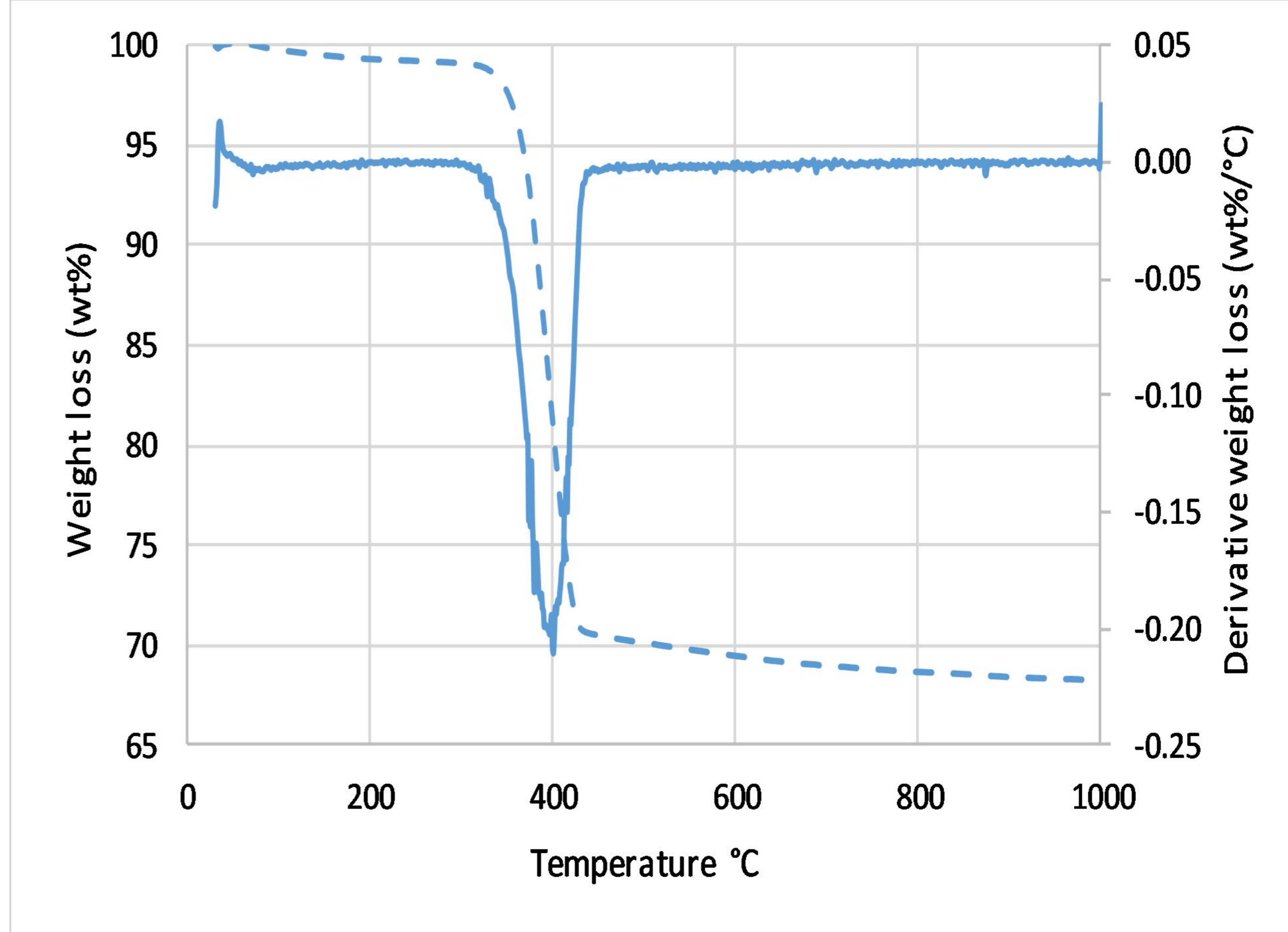
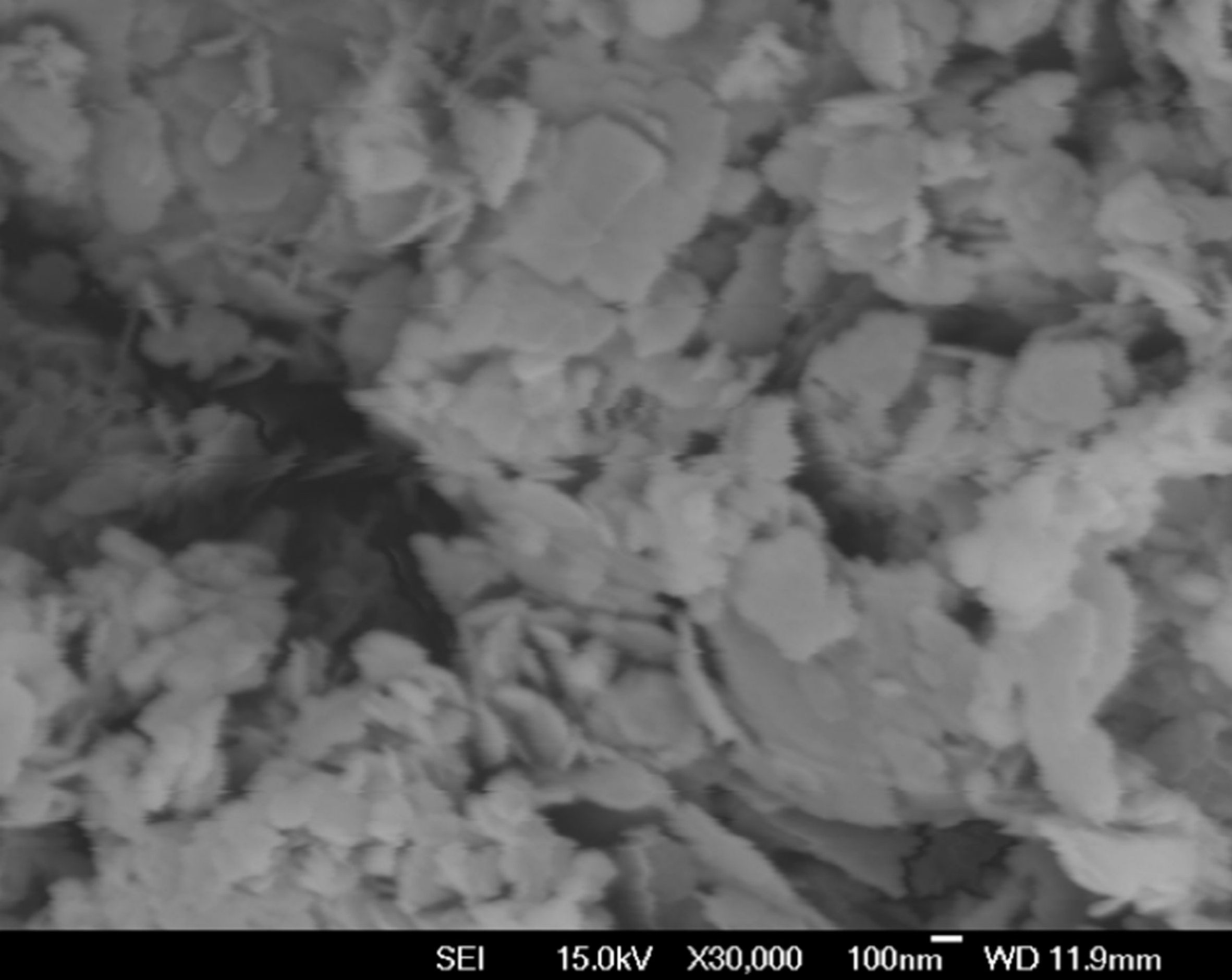
Processing



CO₂ Sequestration

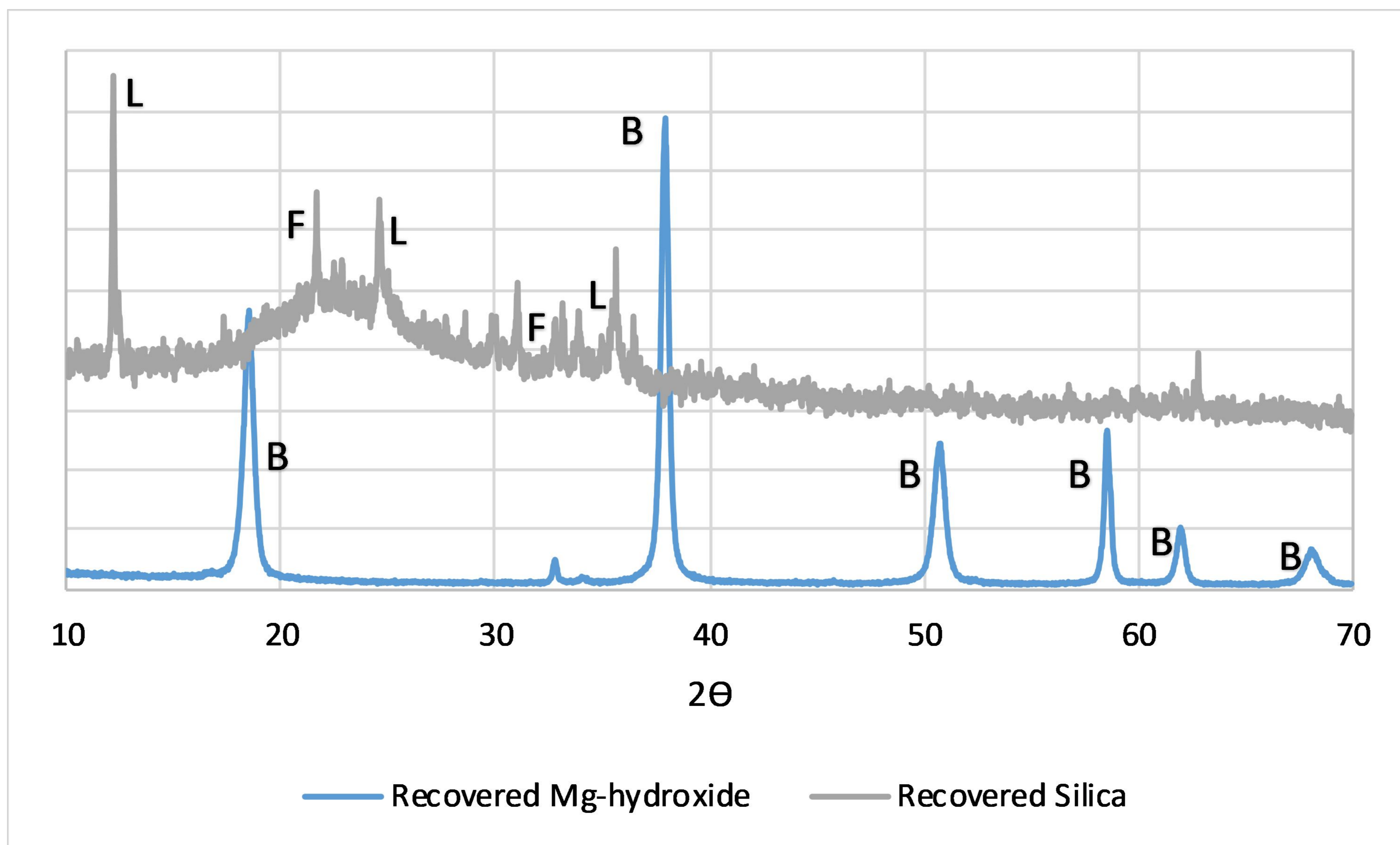


For sequestering 1 tonne of CO₂, 1.3 tonnes of Mg(OH)₂ is required.

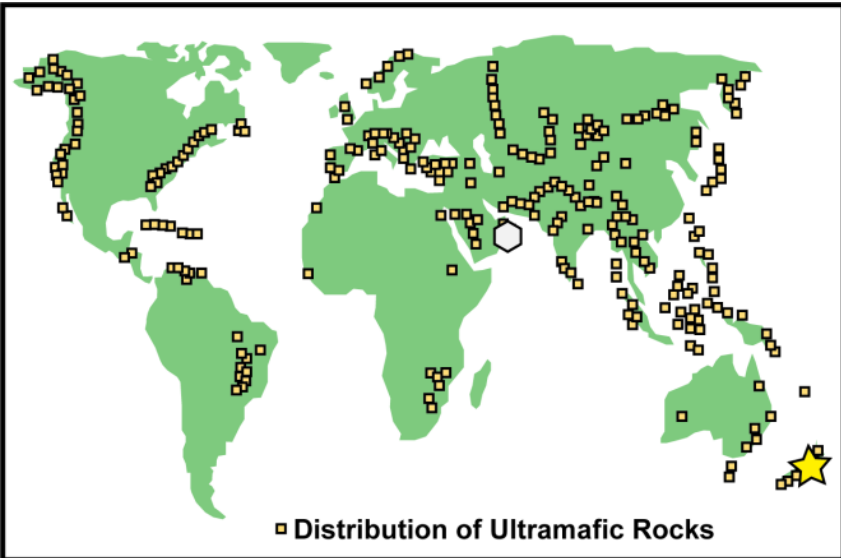


a)

b)



c)



Red Hills, New Zealand ★
 871 Billion Tonnes Olivine (Estimated)
 (Assuming 60% Olivine)



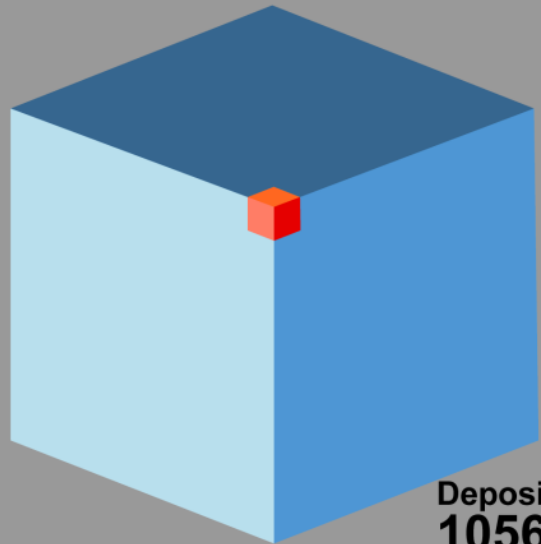
Deposit Lifetime
6.6 years

Billions of tonnes of olivine per year required to:

105 Sequester All Anthropogenic CO₂
 +
26 Global Reduction of 10 Billion Tonnes CO₂

131 Billion Tonnes

Semail Ophiolite, Oman ◻
 1.4x10⁵ Billion Tonnes Olivine (Estimated)
 (Assuming 60% Olivine)



Deposit Lifetime
1056 years

Table 1. Elemental compositions of raw olivine sand and recovered Mg(OH)₂ and silica from olivine, determined by XRF analysis.

	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	Na ₂ O	K ₂ O	LOI	Total
	-----Wt. %-----								
Raw olivine	39.6	0.38	10.7	0.73	45.0	0.14	0	3.2	100.0
Mg(OH) ₂ -olivine	0.1	0.11	6.4	0.30	60.4	0.03	<0.01	32.3	99.9
Silica-olivine	63.2	0.23	4.7	0.57	13.9	0.03	0.06	16.4	99.0